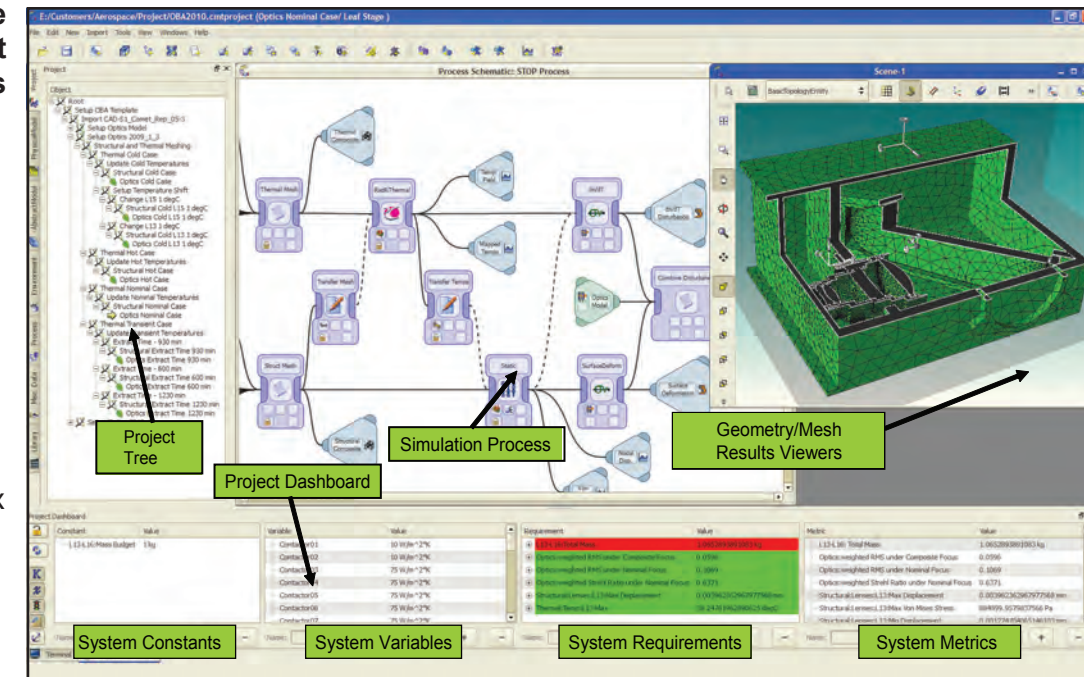


Collaborative Design and Analysis of Electro-Optical Sensors

Comet Solutions™ (www.cometsolutions.com) provides a Performance Engineering Workspace that enables Electro-Optical (EO) sensors, such as telescopes and cameras, to be designed and analyzed in an integrated and collaborative manner across engineering discipline boundaries. This desktop-based software environment enables detailed design and analysis, system engineering and program management to be performed in a single integrated environment with the following features:

- ▶ **Comet™ is configured to work with the CAD and CAE tools that discipline engineers already use to do their work:** PRO/Engineer® or SolidWorks® (mechanical CAD), Abaqus® or MSC NASTRAN™ (structures), Thermal Desktop® (thermal), SigFit (structural to optical conversion), CODE V® (optics), MATLAB® and Excel®.
- ▶ **Design and analysis data for all disciplines is captured in a common data model that anyone can access through Comet.** This allows ready access to all analysis and key performance data.
- ▶ **Project data is efficiently captured and organized in the Comet project.** All analysis data and design variations are captured. Version control is enforced to ensure consistency of design between disciplines.
- ▶ **Interactive problem solving and design reviews are conducted within the Comet environment without the need for PowerPoint snapshots of design status.** Quantitative visualization of CAD/CAE results across discipline boundaries and in a single eye span facilitates discovery and troubleshooting of interdisciplinary design issues.
- ▶ **Model predictions can be easily compared to test results within Comet's workspace.**



Comet's Performance Engineering Workspace also allows complex, interdisciplinary analyses to be developed and captured for reuse as simulation processes.

A Simulation Process effectively integrates complex analyses that were formerly fragmented across engineering discipline boundaries into a single integrated process with a dramatic reduction in design cycle time.

This flier illustrates how Comet software was used by an engineering team for integrated Structural/Thermal/Optical (STOP) analysis at the Aerospace Corp. STOP analysis calculates the optical performance impacts arising from structural deformations to an opto-mechanical system that are caused by quasi-static changes in instrument thermal environment.

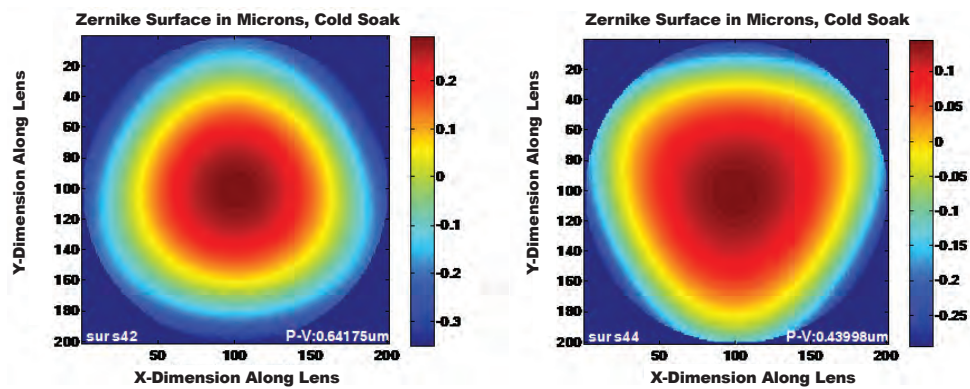
STOP analyses that typically take days to weeks can now be run in a single day.

Design cycle time is reduced by factors of 2X or more and most data handoff errors are eliminated by capturing expertise in Comet simulation templates.

The Comet Project Dashboard provides a single, interactive view of a design's key performance data that auto-

matically updates as the design evolves. System variables are changed directly from the dashboard and the STOP process repeated to conduct parametric studies and improve performance against requirements.

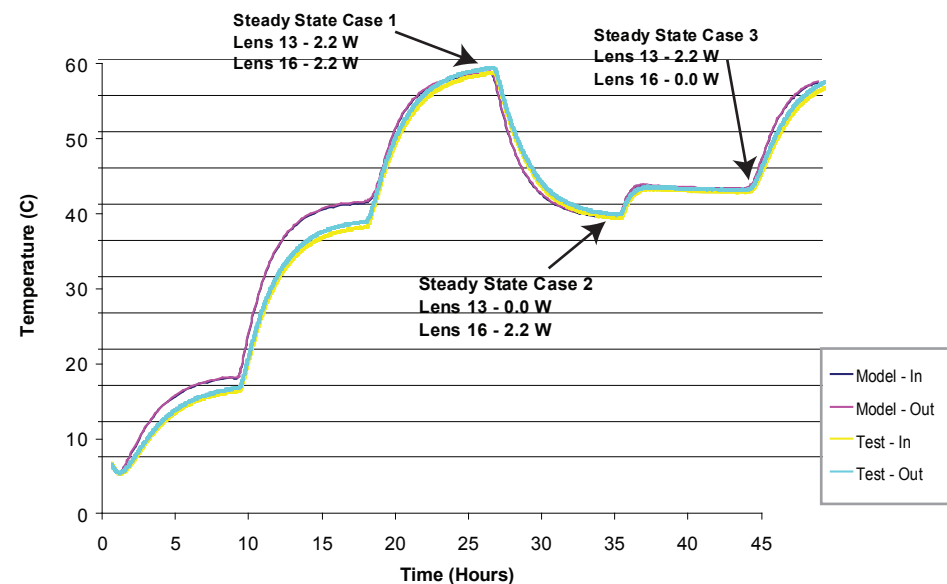
Thermally induced changes in design are readily visualized in the Comet environment. The figures (below) show the wavefront errors introduced by structural deformations to each surface on a single lens in the system and the best fit rigid body tilts and decenters of those surfaces when the system is exposed to a cold soak thermal environment. Comparisons between STOP model



Best fit rigid body displacements of lens surfaces computed by SigFit.

x-decenter	S41	6.14E-05 in	x-decenter	S42	6.17E-05 in
y-decenter	S41	2.43E-05 in	y-decenter	S42	2.56E-05 in
z-decenter	S41	1.87E-04 in	z-decenter	S42	1.21E-04 in
a-tilt	S41	1.17E-04 °	a-tilt	S42	1.19E-04 °
b-tilt	S41	-2.91E-05 °	b-tilt	S42	-4.23E-05 °
c-tilt	S41	-5.79E-04 °	c-tilt	S42	-5.79E-04 °

Lens 13 Center Temperature Comparison: Model vs. Thermal Transient Test Data



Variable	Value	Requirement	Value	Metric	Value
Heater_L16	0.74 W	L13-L16: Total Mass	1.0652893891083 kg	L13-L16: Total Mass	1.0652893891083 kg
Heater_Off	41.1 degC	Optics-weighted RMS under Composite Focus	0.0596	Optics-weighted RMS under Composite Focus	0.0596
Heater_On	40.9 degC	Optics-weighted RMS under Nominal Focus	0.1069	Optics-weighted RMS under Nominal Focus	0.1069
InitialTemperature	20 degC	Optics-weighted Strehl Ratio under Nominal Focus	0.6371	Optics-weighted Strehl Ratio under Nominal Focus	0.6371
Load:L13_PerPad	7.2 lbf	Structural:Lenses:13:Max Displacement	0.003962362967977568 mm	Structural:Lenses:13:Max Displacement	0.003962362967977568 mm
Load:L14_PerPad	7.7 lbf	Structural:Lenses:13:Max Von Mises Stress	884599.9579837566 Pa	Structural:Lenses:13:Max Von Mises Stress	884599.9579837566 Pa
Load:L15_PerPad	3.2 lbf	Structural:Lenses:13:Min Displacement	0.001274704065146103 mm	Structural:Lenses:13:Min Displacement	0.001274704065146103 mm
Load:L16_PerPad	9.9 lbf	Structural:Lenses:14:Max Displacement	0.003110896746920412 mm	Structural:Lenses:14:Max Displacement	0.003110896746920412 mm
OBA_Temperature_Bottom	14 degC	Structural:Lenses:14:Max Von Mises Stress	412399.980412052 Pa	Structural:Lenses:14:Max Von Mises Stress	412399.980412052 Pa
OBA_Temperature_Sides	13 degC	Structural:Lenses:14:Min Displacement	0.002157143681375907 mm	Structural:Lenses:14:Min Displacement	0.002157143681375907 mm
OBA_Temperature_Top	14 degC	Structural:Lenses:15:Max Displacement	0.004284880530423223 mm	Structural:Lenses:15:Max Displacement	0.004284880530423223 mm

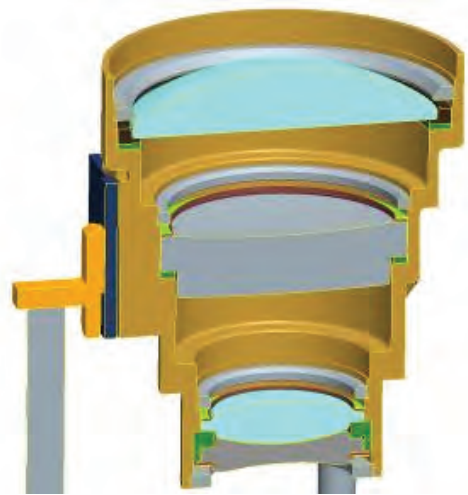
Thermocouple	Model	Test Data	ΔT	abs ΔT
L13_F_S1	35.1	35.4	-0.3	0.3
L13_F_C	35.0	35.0	0.0	0.0
L13_F_S2	35.2	35.1	0.1	0.1
L13_B_S1	35.2	35.5	-0.3	0.3
L13_B_C	35.0	35.2	-0.2	0.2
L13_B_S2	35.2	35.7	-0.4	0.4
L14_F_C	32.2	36.6	-4.4	4.4
L14_F_S2	32.4	36.9	-4.5	4.5
L14_B_S1	32.2	36.8	-4.6	4.6
L14_B_C	32.1	36.6	-4.4	4.4
L14_B_S2	32.2	37.5	-5.4	5.4
L15_F_S2	30.4	34.9	-4.5	4.5
L16_B_S1	29.5	30.8	-1.3	1.3
L16_B_C	29.2	30.6	-1.4	1.4
L16_B_S2	29.5	29.7	-0.2	0.2
H_L13_R1	37.2	43.3	-6.0	6.0
H_L13_R2	36.8	37.2	-0.4	0.4
H_L13_R3	37.2	42.4	-5.2	5.2
H_SOH_R1	32.2	38.5	-6.3	6.3
H_SOH_R2	32.3	38.4	-6.1	6.1
H_SOH_R3	32.3	38.8	-6.5	6.5
H_L16_R1	30.4	34.3	-3.9	3.9
H_L16_R2	30.4	29.6	0.9	0.9

predictions and hardware measurements are readily implemented within the Comet workspace. In the chart above, STOP model temperature predictions at thermocouple monitoring points are compared to transient thermal test results are shown below right.

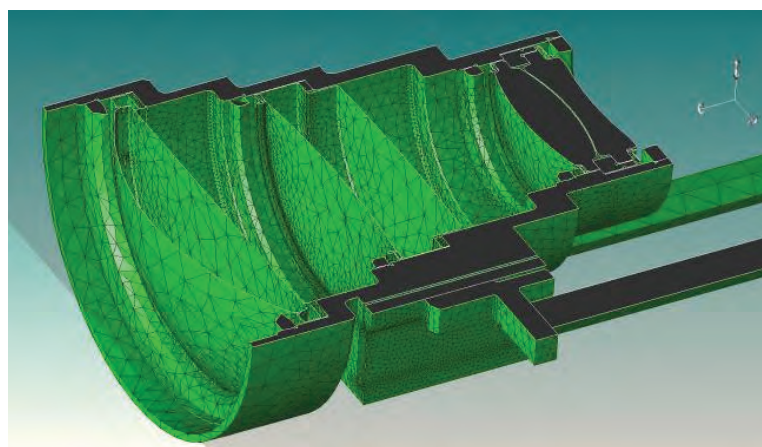


Don Tolle
513-295-3641
don.tolle@cometsolutions.com

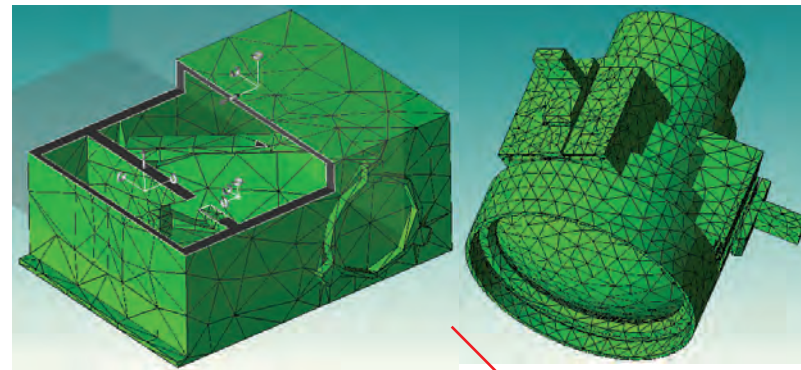
Malcolm Panthaki
505-238-1555
malcolm.panthaki@cometsolutions.com



Step 1: Process starts with a single integrated CAD model for the optical system with tags applied by discipline engineers to parts and subassemblies that will be used for downstream thermal, structural and optical analysis.

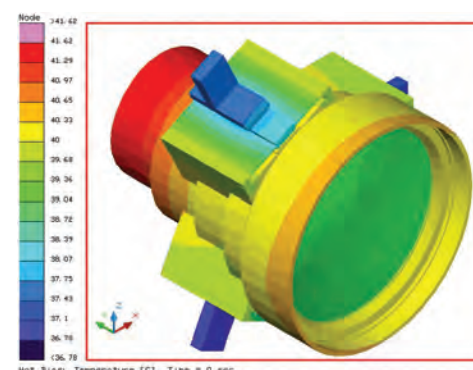


Step 2 (structures): The parts of the CAD model of structural interest are FEM meshed for subsequent analysis using rules that are iteratively developed by the structures engineer and captured in the Comet environment.

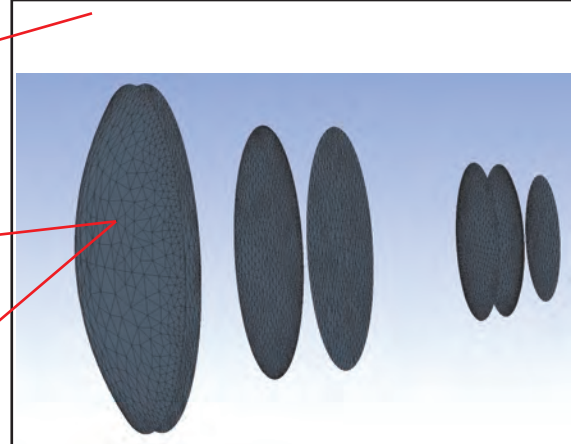
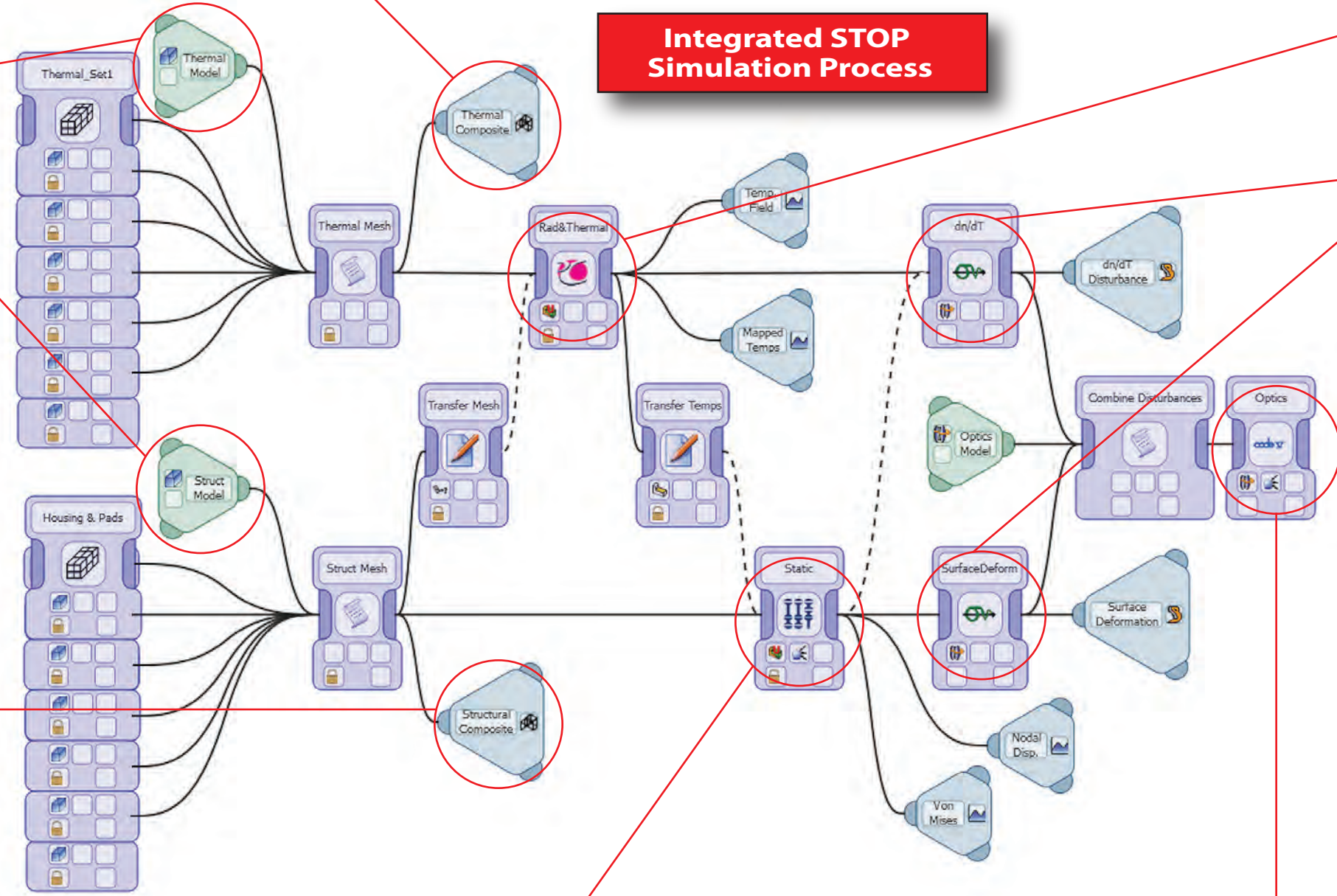


Step 2 (thermal): The parts of the CAD model of thermal interest are FEM meshed for subsequent analysis using rules that are iteratively developed by the thermal engineer and captured in the Comet environment.

Step 3: The meshed thermal model is imported into Thermal Desktop for analysis of temperature distributions subject to boundary conditions and surface properties specified by the thermal engineer and captured in the Comet environment. The temperature field is automatically mapped to the fine structures mesh.

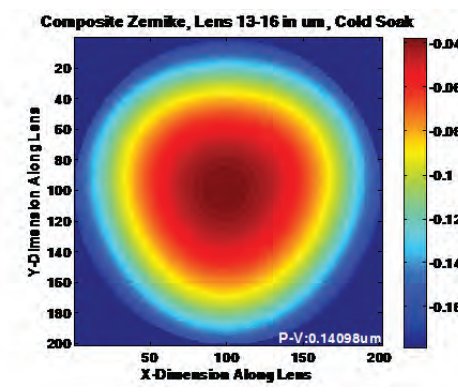
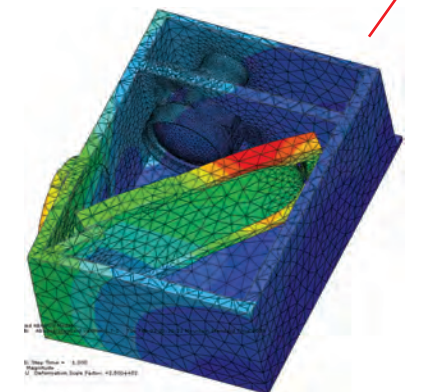
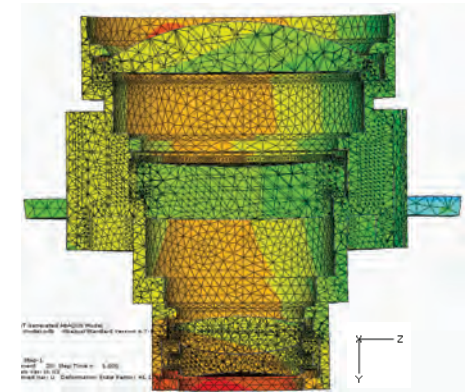


Integrated STOP Simulation Process



Step 5: Temperature fields from Thermal Desktop and structural deformations from Abaqus are imported into SigFit. Sigfit outputs a modified optical design model that represents structural deformations as rigid body component motions plus Zernike polynomial deformations to the optical surfaces. Zernike polynomials are also used to represent wavefront errors introduced by thermal gradients within the lenses.

Step 4: The meshed structures model and the temperature field produced by Thermal Desktop are imported into Abaqus for calculation of structural deformations subject to boundary conditions and material properties specified by the structures engineer and captured in Comet. Lens mount contact stresses are modeled accurately, as shown to the right.



Step 6: CODE V uses the modified optical model output by Sigfit to quantify impacts on optical performance produced by thermally-induced structural deformations and by changes in the refractive indices. An exit pupil wavefront error map is shown at left and a Modulation Transfer Function plot at right.

